



# Robust Control Systems

## Weighted Sensitivity and Performance

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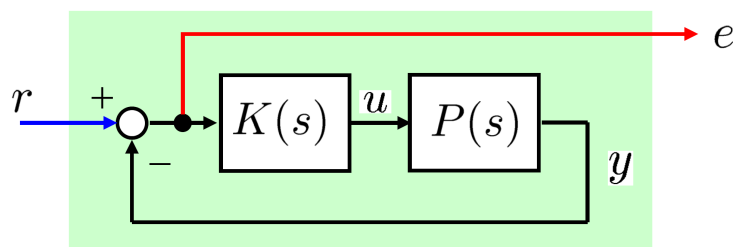
## Reference

1. S. Skogestad and I. Postlethwaite, **Multivariable Feedback Control; Analysis and Design**, Second Edition, Wiley, 2005.
2. M. Fujita, **Lecture Notes on Feedback Control Systems**, Tokyo Institute of Technology, 2019.
3. R. Smith, **Lecture Notes on Control Systems**, ETH Zurich, 2020.
4. H. S. Tsien, **Engineering Cybernetics**, McGraw-Hill, 1954.

## Sensitivity Optimization in Feedback Control

Feedback Performance = Sensitivity

$H^\infty$  norm:  $\min_{\text{Feedback } K} \|S\| = \min_K \|(I + PK)^{-1}\|_\infty$  (System Gain)



$$e = (I + PK)^{-1}r = Sr$$

Sensitivity from Reference to Error

## Bode Sensitivity Integrals (Waterbed Effects) for Stable Plant

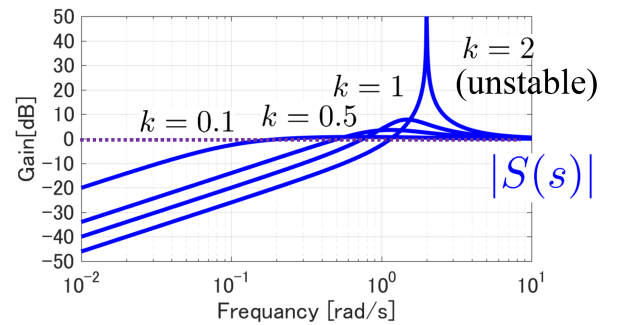
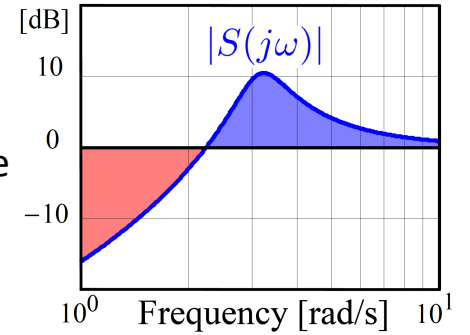
$$\int_0^{\infty} \log |\det S(j\omega)| d\omega = 0 \quad \begin{matrix} |\det S| < 1 \\ |\det S| > 1 \end{matrix}$$

There exists a frequency range over which the magnitude of the sensitivity function exceeds 1 if it is to be kept below 1 at the other frequency range.

**Example:**

$$P(s) = \frac{2-s}{2+s} \quad \text{RHP(Right-Half Plane) Zero}$$

$$K(s) = \frac{k}{s} \quad S(s) = \frac{1}{1 + P(s)K(s)}$$

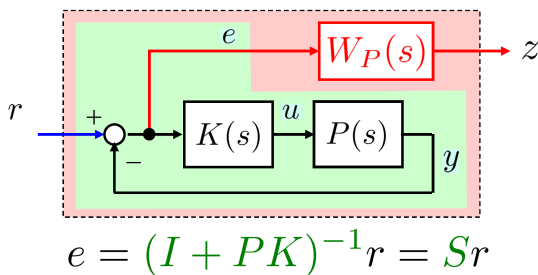


(Ref 1, pp. 167, 170, 223)  
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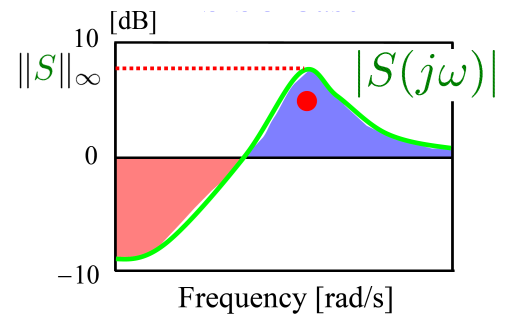
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## Weighted Sensitivity



$\|S\|_{\infty}$  Small?

SISO case: Waterbed Effects



$\|W_P S\|_{\infty}$  Small! Intractable  $\Rightarrow$  Tractable!

**Performance weight**  
transfer function matrix

$$W_P(s) = \begin{bmatrix} w_{p1}(s) & 0 & 0 \\ 0 & \ddots & 0 \\ 0 & 0 & w_{pn}(s) \end{bmatrix} \left( = \begin{bmatrix} w_p(s) & 0 & 0 \\ 0 & \ddots & 0 \\ 0 & 0 & w_p(s) \end{bmatrix} \right)$$

(Ref 1, p. 60)

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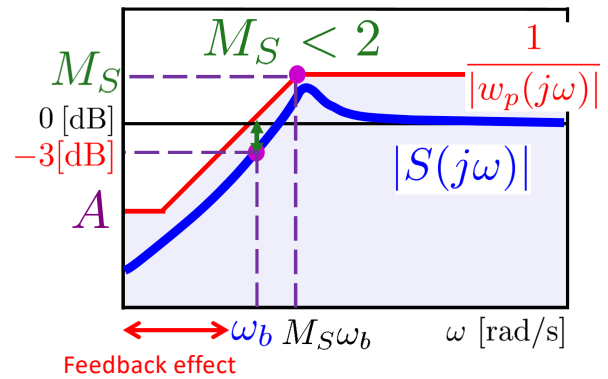
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## Performance Weight

**First-order Performance Weight**

$$w_p(s) = \frac{\frac{1}{M_S} s + \omega_b}{s + \omega_b A}$$

$$w_p(s) = \frac{(s/M_S^{1/n} + \omega_b)^n}{(s + \omega_b A^{1/n})^n}$$



$\omega_b$  : the frequency at which the asymptote of  $1/|w_p(j\omega)|$  crosses 1, and the bandwidth requirement approximately

$M_S$ :  $1/|w_p(j\omega)|$  at high frequencies ( $M_S < 2$ : Rule of thumb)

$A$  :  $1/|w_p(j\omega)|$  at low frequencies

(Ref 1, pp. 62, 80)

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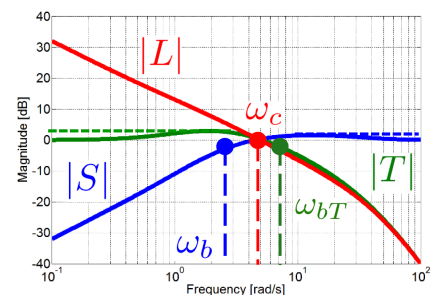
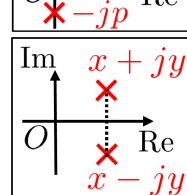
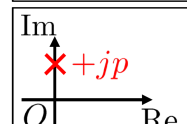
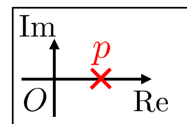
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## Stability and Performance

### Unstable Plant:

- Real RHP Poles:  $2p < \omega_c$
- Imaginary Poles:  $1.15|p| < \omega_c$
- Complex RHP Poles:  $0.67(x + \sqrt{4x^2 + 3y^2}) < \omega_c$

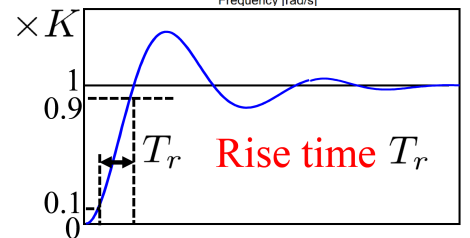


### Stable Plant:

- **First-order System:**

$$G_1(s) = \frac{K}{Ts + 1} \quad K > 0, T > 0$$

$$T_r = (\ln 9)T \approx 2.2T \quad \frac{2.2}{T_r} \leq \frac{1}{T} \leq \omega_c$$



- **Second-order System:**  $G_2(s) = \frac{K\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad \omega_n > 0, \zeta \geq 0$

$$T_r = \frac{\pi/2 + \arcsin \zeta}{\omega_n \sqrt{1 - \zeta^2}} \quad \frac{1.8}{T_r} \leq \omega_r \leq \omega_c$$

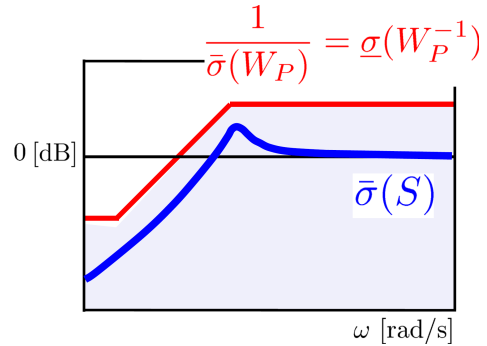
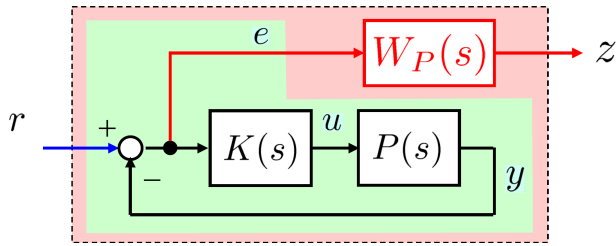
(Ref 1, Sec. 5.9)

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## Nominal Performance (NP)



$$\bar{\sigma}(S(j\omega)) < \frac{1}{\bar{\sigma}(W_P(j\omega))} \quad \forall \omega$$

$$\bar{\sigma}(W_P(j\omega)S(j\omega)) < 1 \quad \forall \omega$$

$$\begin{aligned} \underline{\sigma}(A)\bar{\sigma}(B) &\leq \bar{\sigma}(AB) \\ \bar{\sigma}(AB) &\leq \bar{\sigma}(A)\bar{\sigma}(B) \\ \bar{\sigma}(A^{-1}) &= \frac{1}{\underline{\sigma}(A)} \\ \|A\|_{\infty} &= \bar{\sigma}(A) \end{aligned}$$

○ Nominal Performance (NP) Test:

$$\|W_P(s)S(s)\|_{\infty} < 1$$

(Ref 1, p. 81)

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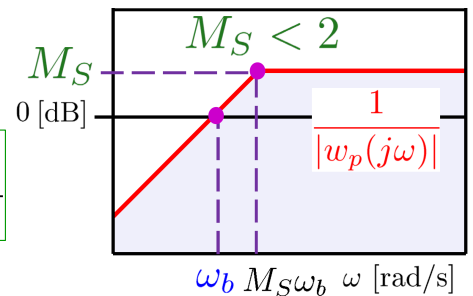
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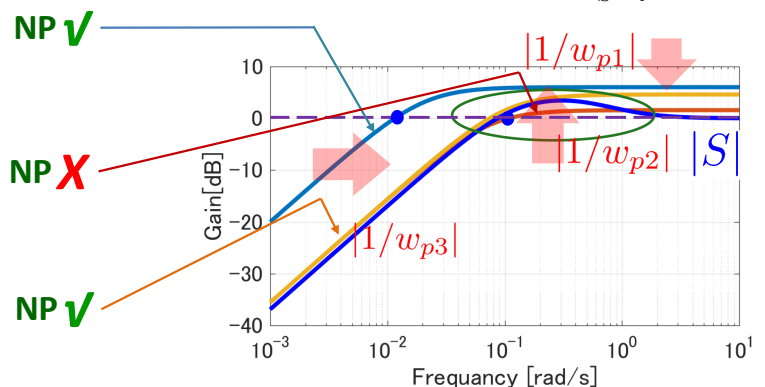
## Nominal Performance Test in SISO Systems

**(NP) Test:**  $|S(j\omega)| < \frac{1}{|w_p(j\omega)|} \quad \forall \omega$

**Example:**  $S = \frac{s^2 + s}{s^2 + 0.7s + 0.07}$        $w_p(s) = \frac{\frac{1}{M_S}s + \omega_b}{s}$



- 1)  $w_{p1} \quad \omega_b = 0.01, M_S = 2$   
↓  $\omega_b$ : fast  $M_S$ : small
- 2)  $w_{p2} \quad \omega_b = 0.06, M_S = 1.2$   
↓  $M_S$ : large
- 3)  $w_{p3} \quad \omega_b = 0.06, M_S = 1.7$



(Ref 1, p. 60)

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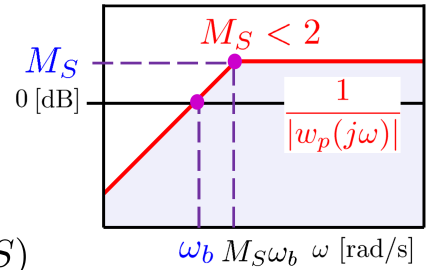
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## Nominal Performance Test in SISO Systems

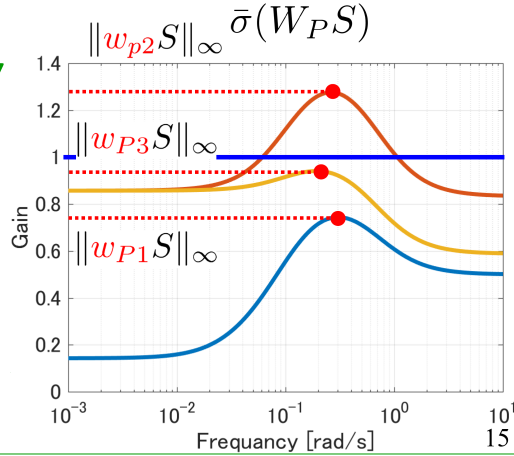
**(NP) Test:**  $\|W_P(s)S(s)\|_\infty < 1$

**Example:**  $S = \frac{s^2 + s}{s^2 + 0.7s + 0.07}$

$w_p(s) = \frac{\frac{1}{M_S}s + \omega_b}{s}$

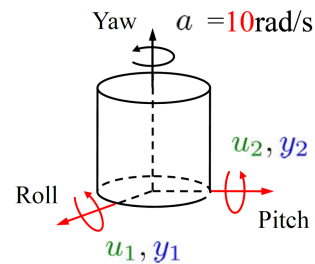


- 1)  $w_{p1} \ \omega_b = 0.01, M_S = 2$  **NP ✓**  
 $\omega_b$ : fast  $M_S$ : small
- 2)  $w_{p2} \ \omega_b = 0.06, M_S = 1.2$  **NP ✗**  
 $M_S$ : large
- 3)  $w_{p3} \ \omega_b = 0.06, M_S = 1.7$  **NP ✓**



## Example: Spinning Satellite

$$P(s) = \begin{bmatrix} P_{11}(s) & P_{12}(s) \\ P_{21}(s) & P_{22}(s) \end{bmatrix} = \begin{bmatrix} \frac{s-100}{s^2+100} & \frac{10s+10}{s^2+100} \\ \frac{-10s-10}{s^2+100} & \frac{s-100}{s^2+100} \end{bmatrix}$$

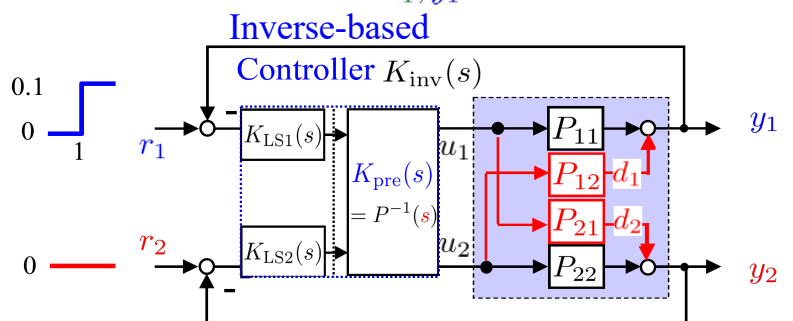


**Inverse-based Controller**  $K_{inv}(s)$  :

$$P^{-1}(s) = 0.01 \begin{bmatrix} s - 100 & -10s - 10 \\ 10s + 10 & s - 100 \end{bmatrix}$$

$$P'(s) = P(s)P^{-1}(s) = I$$

$$K_{inv}(s) = P^{-1}(s) \begin{bmatrix} K_{LS1}(s) & 0 \\ 0 & K_{LS2}(s) \end{bmatrix}$$



**Loop Shaping Design:**  $K_{LS1}(s) = K_{LS2}(s) = \frac{900}{s(s+30)}$  ➔ Desired Loop  $L_{target}(s) = \frac{900}{s(s+30)} I_2$

## Example: Spinning Satellite

### Performance Weight

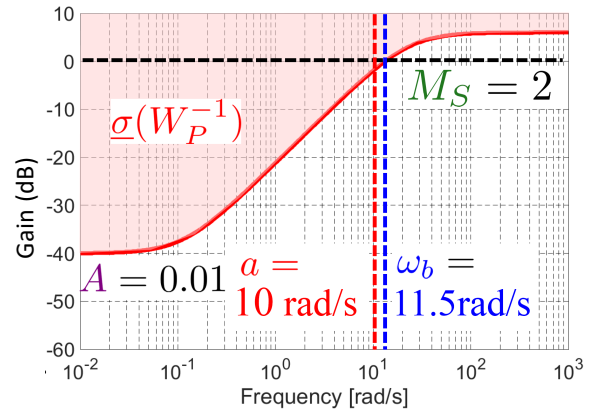
$$W_P(s) = \begin{bmatrix} w_p(s) & 0 \\ 0 & w_p(s) \end{bmatrix} \left( = \begin{bmatrix} w_{p1} & 0 \\ 0 & w_{p2} \end{bmatrix} \right)$$

$$w_p(s) = \frac{1}{M_s} s + \omega_b$$

#### MATLAB Command

```
Ms = 2; A = 1e-2; wb = 11.5;
wP = tf([1/Ms wb], [1 wb*A]);
WP = eye(2)*wP;
figure
sigma(WP)
hold on; grid on;
```

- Poles on the imaginary axis:  $p = \pm a j = \pm 10 j$
- Gain crossover frequency:  
 $\omega_c > 1.15|p| = 11.5 \text{ rad/s} = \omega_b$
- Phase stabilization:  
 $\omega_c < \text{System bandwidth of Actuator/Sensor/Controller}$   
 $M_S \leq 2 \rightarrow M_S = 2$
- Steady state error:  $e \leq 0.01 \rightarrow A = 0.01$



## Example: Spinning Satellite

### Plant:

$$P(s) = \begin{bmatrix} \frac{s-100}{s^2+100} & \frac{10s+10}{s^2+100} \\ \frac{-10s-10}{s^2+100} & \frac{s-100}{s^2+100} \end{bmatrix}$$

### Controller (Inverse-based Controller):

$$K_{\text{inv}}(s) = P^{-1}(s) \begin{bmatrix} \frac{900}{s(s+30)} & 0 \\ 0 & \frac{900}{s(s+30)} \end{bmatrix}$$

Target Loop Transfer Function:  $L(s) = PK_{\text{inv}} = \frac{900}{s(s+30)} I_2$

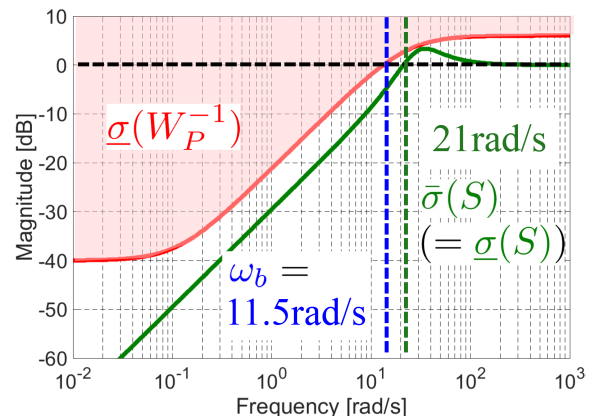
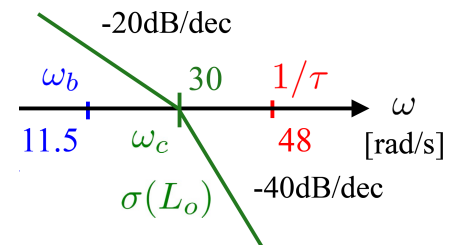
(Output) Sensitivity Function:  $S(s) = (I + PK_{\text{inv}})^{-1}$

➔

$$\|W_P S\|_{\infty} = 0.8935 < 1 \quad \text{NP } \checkmark$$

#### MATLAB Command

```
KI = inv(Pnom)*tf([1],[1 30 0])*diag([900 900]);
FI = loopsens(Pnom,KI);
sigma(FI.So);
hinfSo = normhinf(WP*FI.So)
```



## Optimal Sensitivity Minimization Problem

Find a stabilizing controller  $K$  which make smaller (**minimize**)

$$\|W_P(s)S(s)\|_\infty$$

↓ Intractable

**Sensitivity Minimization Problem (H $\infty$  Control)**

Given  $\gamma > \gamma_{min}$ , find all stabilizing controllers  $K$  such that

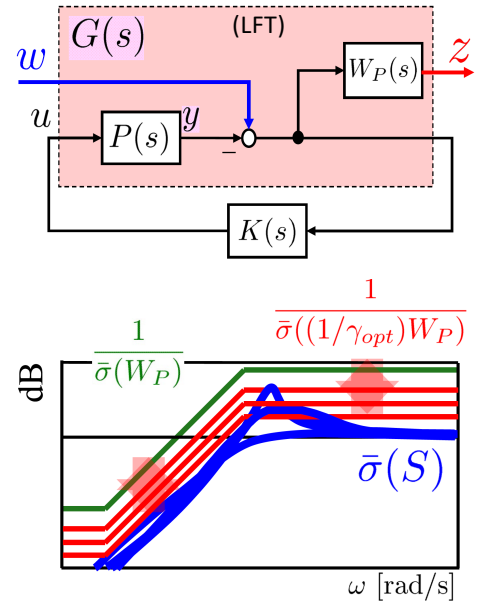
$$\|W_P(s)S(s)\|_\infty < \gamma$$

1)  $\|W_P S\|_\infty < \gamma_1$  ✓  $\exists K_1$

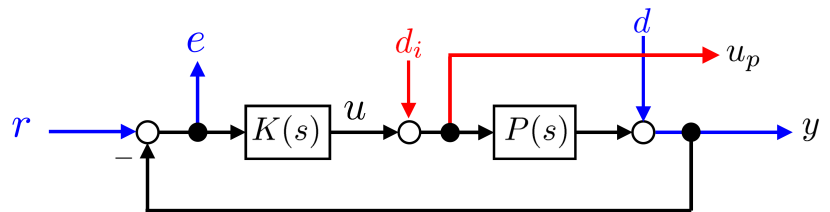
2)  $\|W_P S\|_\infty < \gamma_2$  ✗ no  $K_2$

3)  $\|W_P S\|_\infty < \gamma_3$  ✓  $\exists K_3$

⋮  
 $\frac{1}{\gamma_{opt}} W_P$



## Sensitivity for MIMO Systems



○ Sensitivity to Output Disturbance  $d$  :

Output Sensitivity Function:  $S_o(s) = (I + P(s)K(s))^{-1}$

○ Sensitivity to Input Disturbance  $d_i$  :

Input Sensitivity Function:  $S_i(s) = (I + K(s)P(s))^{-1}$

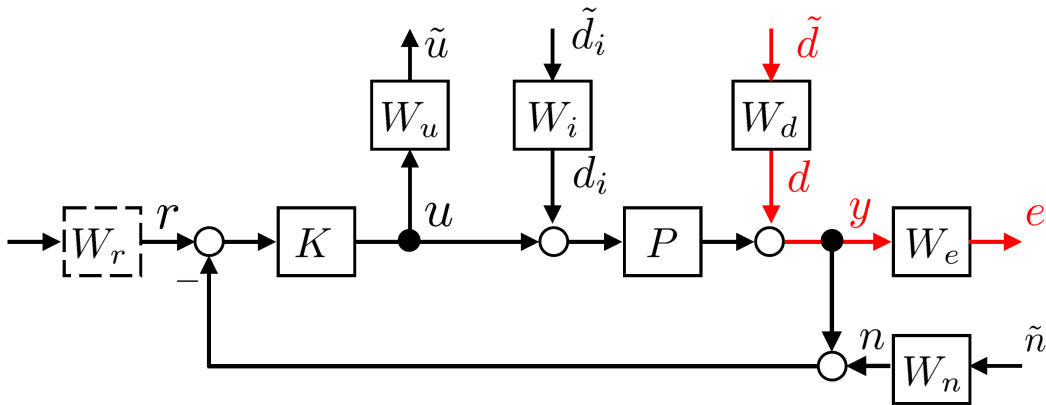
For SISO Systems:  $S_i = S_o$

but for MIMO Systems:  $PK \neq KP \rightarrow S_i \neq S_o$

Good disturbance rejection at output does not always mean good rejection at input



## Standard Feedback Configuration with Weights



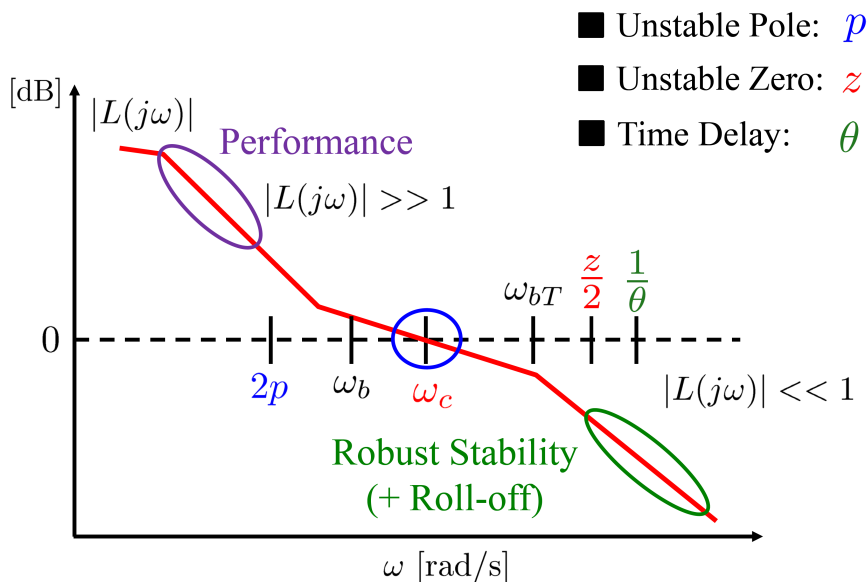
### o Sensitivity Minimization Problem

find  $K(s)$  s.t.  $\|W_e(s)S_o(s)W_d(s)\|_\infty < \gamma$

(Ref 1, p. 363)

## SISO Loop Shaping

**Loop Shaping:** Gives us graphical interpretation (Bode Plot, and System Gain)



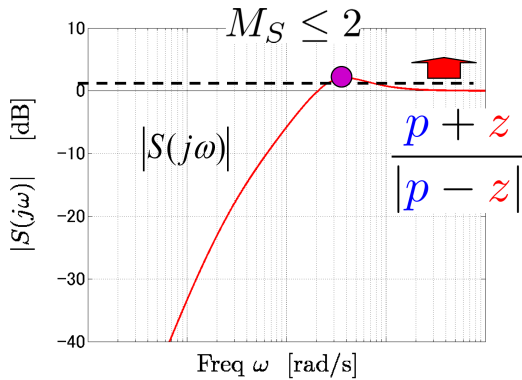
(Ref 1, pp. 41, 42, 343)

# RHP Poles/Zeros, Time Delays and Sensitivity (SISO Systems)

For systems with a RHP pole  $p$  and RHP zero  $z$  (or a time delay  $\theta$ ), any stabilizing controller gives sensitivity functions with the property

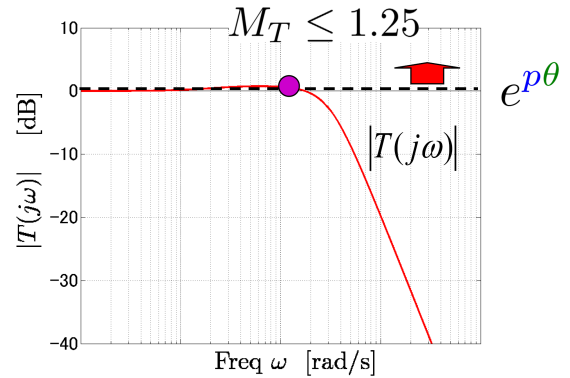
$$M_S = \sup_{\omega} |S(j\omega)| \geq \frac{p+z}{|p-z|}$$

The zero and the pole must be sufficiently far apart



$$M_T = \sup_{\omega} |T(j\omega)| \geq e^{p\theta}$$

The product of RHP pole and time delay must be sufficiently small



# Norms

## Key properties:

1. Non-negative
2. Positive
3. Homogeneous
4. Triangle inequality

$$\|e\| \geq 0$$

$$\|e\| = 0 \text{ iff } e = 0$$

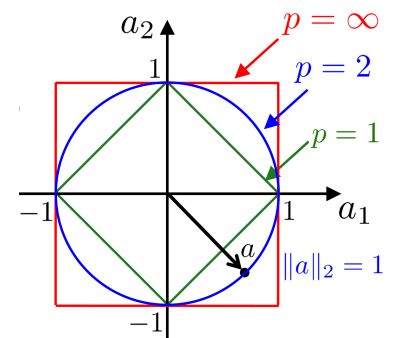
$$\|\alpha e\| = |\alpha| \|e\|, \forall \alpha : \text{scalar}$$

$$\|e_1 + e_2\| \geq \|e_1\| + \|e_2\|$$

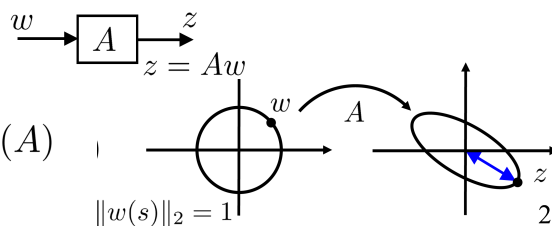
## Vector Norm (Ex.)

$$\|a\|_2 = \sqrt{\sum_i |a_i|^2} \quad (\text{Euclidean Vector Norm})$$

$$\|a\|_1 = \sum_i |a_i|, \quad \|a\|_\infty = \max_i |a_i|$$



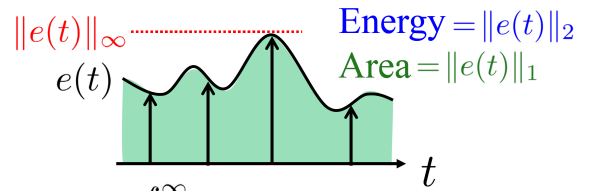
## (Induced) Matrix Norm



$$\text{Ex.: } \|A\|_{i2} = \max_{\omega \neq 0} \frac{\|z\|_2}{\|\omega\|_2} = \bar{\sigma}(A)$$

## Norms

### ○ Signal Norm



#### Examples:

○ “Energy of signal” ( $\mathcal{L}_2$ -norm,  $\mathcal{L}$ : Lebesgue space)  $\|e(t)\|_2^2 = \int_{-\infty}^{\infty} \sum_i |e_i(t)|^2 dt$

○ Integral absolute error  $\|e(t)\|_1 = \int_{-\infty}^{\infty} \sum_i |e_i(t)| dt$

○ “maximum value over time”  $\|e(t)\|_{\infty} = \max_t \left( \max_i |e_i(t)| \right)$

**System Norm (MIMO):**  $\|G(s)\|_{\infty} = \max_{\omega \neq 0} \frac{\|z\|_2}{\|w\|_2} = \max_{\omega} \bar{\sigma}(G(j\omega))$  (System Gain)  $w \rightarrow \boxed{G(s)} \rightarrow z$

$$\|G(s)\|_2 = \sqrt{\frac{1}{2\pi} \int_{-\infty}^{\infty} \text{tr}(G(j\omega)^H G(j\omega)) d\omega} = \sqrt{\frac{1}{2\pi} \int_{-\infty}^{\infty} \sum_i \sigma_i^2(G(j\omega)) d\omega}$$

(Ref 1, A.5)

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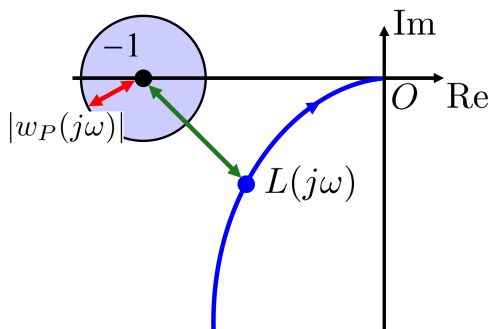
## Nominal Performance in SISO Systems

$$|w_P S| < 1 \quad \forall \omega \quad \Leftrightarrow \quad |w_P| < |1 + L| \quad \forall \omega$$

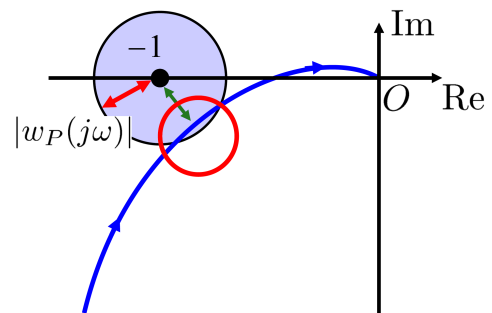
$$S = \frac{1}{1 + PK} = \frac{1}{1 + L}$$

### ○ Nyquist Plot

L should be away from (-1, 0) by  $|w_P|$



$$|w_P| < |1 + L| \quad \forall \omega \quad \checkmark$$



$$|w_P| > |1 + L| \quad \exists \omega \quad \times$$

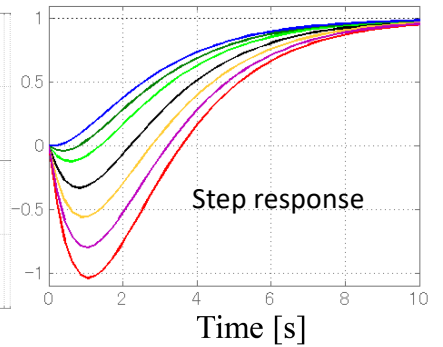
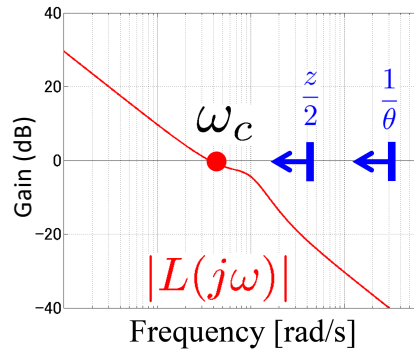
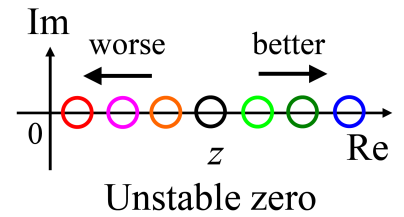
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## Fundamental Limitations

- Bound on the Crossover Frequency  $\omega_c$
- RHP (Right half-plane) Zero  $z$   $\omega_c < \frac{z}{2}$
- Fast RHP Zeros ( $z$  large): **Loose** Restrictions
- Slow RHP Zeros ( $z$  small): **Tight** Restrictions
- Time delay  $\theta$ :  $\omega_c < \frac{1}{\theta}$



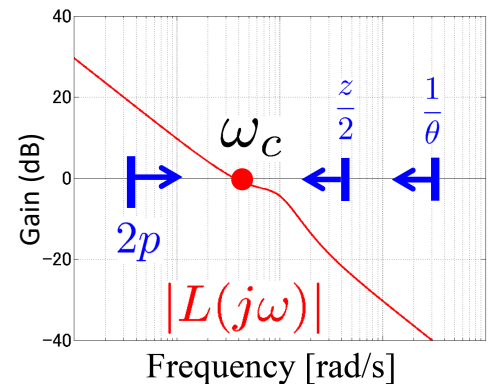
(Ref 1, p. 183)  
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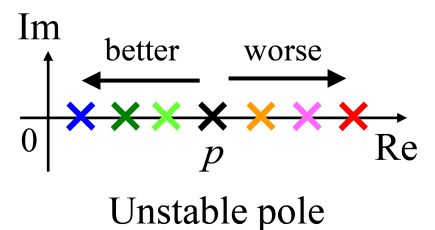
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## Fundamental Limitations

- Bound on the Crossover Frequency  $\omega_c$
- RHP (Right half-plane) Poles  $p$   $\omega_c > 2p$
- Slow RHP Poles ( $p$  small): **Loose** Restrictions
- Fast RHP Poles ( $p$  large): **Tight** Restrictions



Poles on imaginary axis:  $\pm pj$   $\omega_c > 1.15|p|$



(Ref 1, pp. 192, 194)  
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## Fundamental Limitations in MIMO Systems

- Algebraic Constraint

$$S + T = I$$

$$\begin{aligned} |\bar{\sigma}(S) - 1| &\leq \bar{\sigma}(T) \leq \bar{\sigma}(S) + 1 \\ |\bar{\sigma}(T) - 1| &\leq \bar{\sigma}(S) \leq \bar{\sigma}(T) + 1 \end{aligned}$$



$$|\bar{\sigma}(S) - \bar{\sigma}(T)| \leq 1$$

$\bar{\sigma}(S)$  is large if and only if  $\bar{\sigma}(T)$  is large

- Bounds on Peaks

$$M_{S,\min} \triangleq \min_K \|S\|_\infty, \quad M_{T,\min} \triangleq \min_K \|T\|_\infty$$

(Ref 1, Sec. 6.2)

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## Thank You!



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