





The *Takagi-Sugeno-Kang fuzzy system* is constructed from the following fuzzy IF-THEN rules:





The final output of the Takagi-Sugeno fuzzy system can be inferred as the weighted average of the:



in which the weights are calculated as follows:

$$w^{l} = \prod_{i=1}^{n} \mu_{A_{i}^{l}}(x_{i})$$



This kind of fuzzy systems can be employed to represent nonlinear plant by local linear model. Consider a continuous nonlinear system of the following state space form:

 $\begin{cases} \dot{x}(t) = f\left(x(t), u(t)\right) \\ y(t) = h\left(x(t), u(t)\right) \end{cases}$

The local linear model of fuzzy IF-THEN rules can be written as follows:

 $Ru^{(l)}: IF \ z_1 \ is \ F_1^l \ and \ ... \ and \ z_k \ is \ F_k^l \ THEN \begin{cases} \dot{x}(t) = A_l x(t) + B_l u(t) \\ y(t) = C_l x(t) + D_l u(t) \end{cases}$

Where $Z_1, ..., Z_k$ denote known premise variables that may be functions of the state variables, and $F_1^l, ..., F_k^l$ are fuzzy sets characterized by fuzzy membership functions.



The final outputs of the fuzzy systems are inferred as follows:

$$\begin{cases} \dot{x}(t) = \sum_{l=1}^{N} \mu_l(z) \left(A_l x(t) + B_l u(t) \right) \\ y(t) = \sum_{l=1}^{N} \mu_l(z) \left(C_l x(t) + D_l u(t) \right) \end{cases}$$

Where N is the number of rule, $z = [z_1, ..., z_k]^T$ is the vector of fuzzy inputs and $\mu_l(z)$ is a fuzzy basis function:

$$\mu_l(z) = \frac{\prod_{i=1}^k F_i^l(z_i)}{\sum_{l=1}^N \prod_{i=1}^k F_i^l(z_i)}$$

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Example: Consider the following nonlinear system:

$$\begin{cases} \dot{x}_1 = -x_1 + x_1 x_2^3 \\ \dot{x}_2 = -x_2 + (3 + x_2) x_1^3 \end{cases}$$

To construct a fuzzy local linear model, It is assumed that $x_1, x_2 \in [-1, +1]$. This nonlinear model can be easily rewritten as follows:





----: To obtain the local linear model of the considered nonlinear system, the following fuzzy IF-THEN rules can be employed:

$$Ru^{(1)}: IF z_1 is F_1 and z_2 is G_1 THEN \dot{x}(t) = A_1 x(t)$$

$$Ru^{(2)}: IF z_1 is F_1 and z_2 is G_2 THEN \dot{x}(t) = A_2 x(t)$$

$$Ru^{(3)}: IF z_1 is F_2 and z_2 is G_1 THEN \dot{x}(t) = A_3 x(t)$$

$$Ru^{(4)}: IF z_1 is F_2 and z_2 is G_2 THEN \dot{x}(t) = A_4 x(t)$$



----: Now, calculate the minimum and maximum of the chosen premise variables:

$$x_1 \in [-1, +1]$$

$$x_2 \in [-1, +1]$$

$$\min\left\{z_{1} = x_{1}x_{2}^{2}\right\} = -1 \qquad \max\left\{z_{1} = x_{1}x_{2}^{2}\right\} = +1$$
$$\min\left\{z_{2} = (3 + x_{2})x_{1}^{2}\right\} = 0 \qquad \max\left\{z_{2} = (3 + x_{2})x_{1}^{2}\right\} = 4$$



----: Accordingly, the matrices A_1, A_2, A_3 and A_4 can be given as:







----: Consequently, the grades of membership of the premise variables are obtained as follows:

$$\min \{z_1\} = -1 \max \{z_1\} = +1$$

$$\sum z_1 = (+1)F_1(z_1) + (-1)F_2(z_1) \min \{z_2\} = 0 \max \{z_2\} = +4$$

$$\sum z_2 = (+4)G_1(z_2) + (0)G_2(z_2)$$

where

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 $F_{1}(z_{1}) + F_{2}(z_{1}) = 1$ $G_{1}(z_{2}) + G_{2}(z_{2}) = 1$



<u>----</u>: Then, by solving the obtained equations, the membership functions are as follows:





<u>----</u>: It can be checked that the designed fuzzy systems exactly represents the nonlinear system in the interval $[-1, +1] \times [-1, +1]$:



with

$$\mu_{1}(z_{1}, z_{2}) = F_{1}(z_{1})G_{1}(z_{2})$$
$$\mu_{2}(z_{1}, z_{2}) = F_{1}(z_{1})G_{2}(z_{2})$$
$$\mu_{3}(z_{1}, z_{2}) = F_{2}(z_{1})G_{1}(z_{2})$$
$$\mu_{4}(z_{1}, z_{2}) = F_{2}(z_{1})G_{2}(z_{2})$$



Assignment: Consider the following nonlinear system:

$$\begin{cases} \dot{x}_1 = -x_1 + x_1 x_2^3 \\ \dot{x}_1 = -x_2 + (3 + x_2) x_1^3 \end{cases}$$

assume that $x_1, x_2 \in [-\alpha, \alpha]$.



To stabilize systems represented by T-S fuzzy systems of the following form:

$$Ru^{(l)}$$
: IF z_1 is F_1^l and and z_k is F_k^l THEN $\dot{x}(t) = A_l x(t) + B_l u(t)$

the parallel distributed compensator controller is defined as:

$$Ru^{(m)}$$
: IF z_1 is F_1^m and and z_k is F_k^m THEN $u(t) = K_m x(t)$

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By applying the parallel distributed compensator control law to local linear model, the closed loop system is obtained by:

$$\dot{x}(t) = \sum_{m=1}^{N} \sum_{l=1}^{N} \mu_m(z) \mu_l(z) \left(A_l + B_l K_m \right) x(t)$$

which can be represented as follows:

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$$\dot{x}(t) = \sum_{l=1}^{N} \left(\mu_{l}(z)\right)^{2} G_{ll} x(t) + \sum_{l=1}^{N} \sum_{l < m}^{N} \mu_{m}(z) \mu_{l}(z) \left(G_{lm} + G_{ml}\right) x(t)$$

with

$$G_{lm} = A_l + B_l K_m$$

Theorem: The equilibrium of closed loop fuzzy system is asymptotically stable if there exist a symmetric matrix P>0 such that:

 $G_{ll}^T P + P G_{ll} < 0$

$$\left(\frac{G_{lm} + G_{ml}}{2}\right)^T P + P\left(\frac{G_{lm} + G_{ml}}{2}\right) \le 0 \quad , \ l < m$$

For $\mu_m(z(t))\mu_l(z(t)) \neq 0, \forall t \text{ and } l, m = 1, 2, ..., N$.

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According to the theorem, the following linear matrix inequalities (LMIs) should be solved to design parallel distributed compensator:

$$-XA_l^T - A_l X + M_l^T B_l^T + B_l M_l > 0$$

$$-XA_{l}^{T} - A_{l}X - XA_{m}^{T} - A_{m}X + M_{m}^{T}B_{l}^{T} + B_{l}M_{m} + M_{l}^{T}B_{m}^{T} + B_{m}M_{l} \ge 0$$
$$X > 0$$

Then the controller gains is obtained:

$$P = X^{-1}$$
 and $K_l = M_l X^{-1}$

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Inverted Pendulum System

The dynamic equations of the nonlinear inverted pendulum system are as follows:

$$\dot{x}_{1}(t) = x_{2}(t)$$

$$\dot{x}_{2}(t) = \frac{gsin(x_{1}(t)) - \frac{amlx_{2}^{2}(t)sin(2x_{1}(t))}{2}}{\frac{4l}{3} - amlcos^{2}(x_{1}(t))} + \frac{-acos(x_{1}(t))}{\frac{4l}{3} - amlcos^{2}(x_{1}(t))} .u(t)$$

where $a = \frac{1}{(M+m)}$; $x_1(t)$ and $x_2(t)$ are respectively the angle and the angular velocity of the pendulum.

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Inverted Pendulum System

It can be shown that this nonlinear system can be approximated by the following two rules:

$$Ru^{(1)}: IF x_1 is about 0 THEN \dot{x}(t) = A_1 x(t) + B_1 u(t)$$

$$Ru^{(2)}: IF x_1 is about \frac{\pm \pi}{2} THEN \dot{x}(t) = A_2 x(t) + B_2 u(t)$$
with
$$\begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix}$$

$$A_{1} = \begin{bmatrix} \frac{g}{4l} & 0 \end{bmatrix} \quad A_{2} = \begin{bmatrix} \frac{2g}{\pi\left(\frac{4l}{3} - aml\beta^{2}\right)} & 0 \end{bmatrix} \quad B_{1} = \begin{bmatrix} -\frac{a}{4l} & -\frac{aml\beta^{2}}{3} \end{bmatrix} \quad B_{2} = \begin{bmatrix} -\frac{a\beta}{4l} & -\frac{aml\beta^{2}}{3} \end{bmatrix}$$

 $\beta = \cos(88^\circ)$

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Inverted Pendulum System

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Accordingly, by solving the following linear matrix inequality:

$$-XA_{1}^{T} - A_{1}X + M_{1}^{T}B_{1}^{T} + B_{1}M_{1} > 0$$

$$-XA_{2}^{T} - A_{2}X + M_{2}^{T}B_{2}^{T} + B_{2}M_{2} > 0$$

$$-XA_{1}^{T} - A_{1}X - XA_{2}^{T} - A_{2}X + M_{2}^{T}B_{1}^{T} + B_{1}M_{2} + M_{1}^{T}B_{2}^{T} + B_{2}M_{1} \ge 0$$

$$X = X^{T} > 0$$
the controller gains is given by:
$$K_{1} = \begin{bmatrix} 0 \end{bmatrix} \text{ and } K_{2} = \begin{bmatrix} 0 \end{bmatrix}$$

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Finally, simulation result is as foolows:

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