



Linear Control System

Steady-State Error and Stability

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Contents

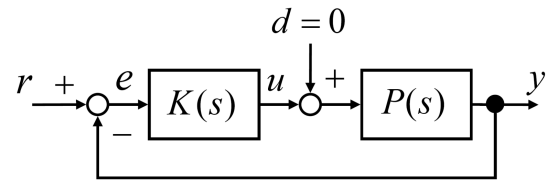
- Steady-State Error
- Stability

Error in Feedback Systems

$$e(t) = r(t) - y(t)$$

$$L(s) = P(s)K(s)$$

$$y(s) = L(s)e(s)$$



$$e(s) = r(s) - L(s)e(s) \Rightarrow (1 + L(s))e(s) = r(s) \Rightarrow e(s) = \frac{1}{1 + L(s)} r(s)$$

$$e_s = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} s \cdot e(s) = \lim_{s \rightarrow 0} s \frac{1}{1 + L(s)} r(s)$$

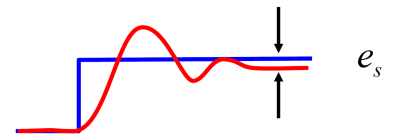
$$\lim_{t \rightarrow \infty} f(t) = \lim_{s \rightarrow 0} sF(s)$$

$$F(s) := \int_0^{\infty} f(t)e^{-st} dt$$

Steady-State Error

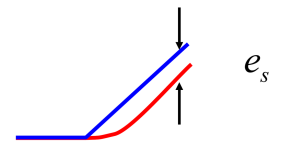
$$r(t) = 1 \quad \left(r(s) = \frac{1}{s} \right) \Rightarrow e_s = \lim_{s \rightarrow 0} s \frac{1}{1 + L(s)} \cdot \frac{1}{s} = \frac{1}{1 + \lim_{s \rightarrow 0} L(s)}$$

$$K_p = \lim_{s \rightarrow 0} L(s) = L(0)$$



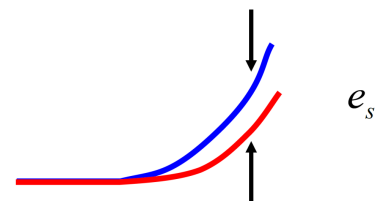
$$r(t) = t \quad \left(r(s) = \frac{1}{s^2} \right) \Rightarrow e_s = \lim_{s \rightarrow 0} s \frac{1}{1 + L(s)} \cdot \frac{1}{s^2} = \lim_{s \rightarrow 0} \frac{1}{sL(s)}$$

$$K_v = \lim_{s \rightarrow 0} sL(s)$$



$$r(t) = \frac{1}{2}t^2 \quad \left(r(s) = \frac{1}{s^3} \right) \Rightarrow e_s = \lim_{s \rightarrow 0} \frac{1}{s^2 L(s)}$$

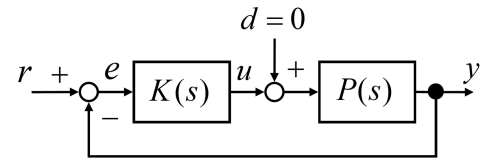
$$K_a = \lim_{s \rightarrow 0} s^2 L(s)$$



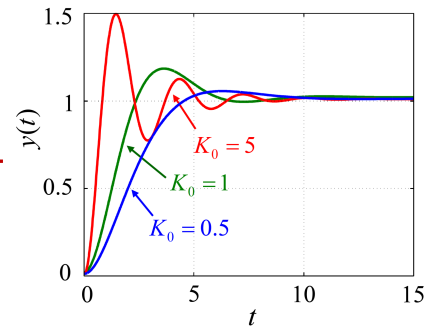
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$$L(s) = P(s)K(s) = \frac{K_0}{s(s+1)}$$

$$P(s) = \frac{1}{s}, \quad K(s) = \frac{K_0}{s+1} \quad (K_0 > 0)$$

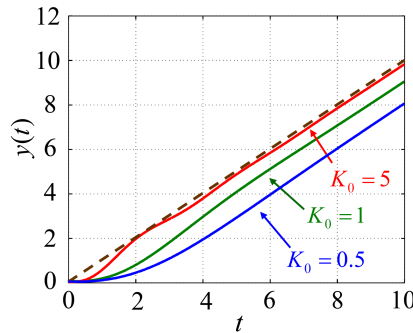


$$K_p = L(0) = \infty \Rightarrow e_s = \frac{1}{1 + \lim_{s \rightarrow 0} L(s)} = \frac{1}{1 + L(0)} = \frac{1}{1 + K_p} = 0$$



$$K_v = \lim_{s \rightarrow 0} sL(s) = \lim_{s \rightarrow 0} s \frac{K_0}{s(s+1)} = K_0$$

$$\Rightarrow e_s = \lim_{s \rightarrow 0} \frac{1}{sL(s)} = \frac{1}{K_0}$$



System Type

$$L(s) = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_0}{s^l (s^n + a_{n-1} s^{n-1} + \dots + a_0)}$$

$$l = 1 \Rightarrow K_p = L(0) = \infty \Rightarrow \frac{1}{1 + K_p} = 0$$

$$l = 2 \Rightarrow K_v = \lim_{s \rightarrow 0} s \cdot L(s) = \infty \Rightarrow \frac{1}{K_v} = 0$$

$$l = 3 \Rightarrow K_a = \lim_{s \rightarrow 0} s^2 \cdot L(s) = \infty \Rightarrow \frac{1}{K_a} = 0$$

$r(t)$ Type	$r(t) = 1$	$r(t) = t$	$r(t) = \frac{t^2}{2}$
0	$\frac{1}{1 + K_p}$	∞	∞
1	0	$\frac{1}{K_v}$	∞
2	0	0	$\frac{1}{K_a}$

System Type

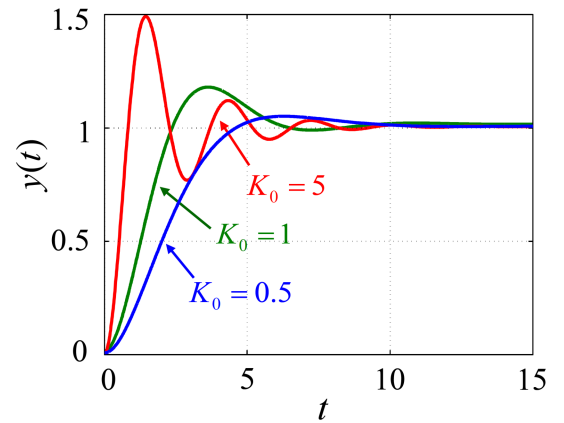
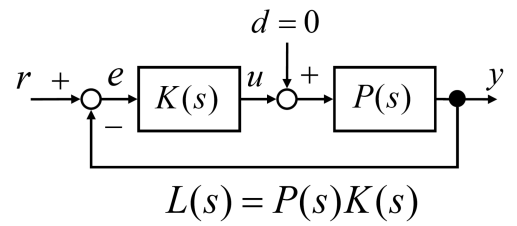
$$e(t) = r(t) - y(t) \Rightarrow e(s) = \frac{1}{1+L(s)} r(s)$$

$$\begin{aligned} e_s &= \lim_{t \rightarrow \infty} e(t) \\ &= \lim_{s \rightarrow 0} s \cdot e(s) \\ &= \lim_{s \rightarrow 0} s \frac{1}{1+L(s)} r(s) \end{aligned}$$

$$K_p = \lim_{s \rightarrow 0} L(s) = L(0)$$

$$K_v = \lim_{s \rightarrow 0} sL(s)$$

$$K_a = \lim_{s \rightarrow 0} s^2 L(s)$$



Example: $P(s) = \frac{1}{s}, K(s) = \frac{K_0}{s+1} \quad (K_0 > 0)$

$$L(s) = P(s)K(s) = \frac{K_0}{s(s+1)} \quad K_p = L(0) = \infty$$

$$\Rightarrow e_s = \frac{1}{1 + \lim_{s \rightarrow 0} L(s)} = \frac{1}{1 + L(0)} = \frac{1}{1 + K_p} = 0$$

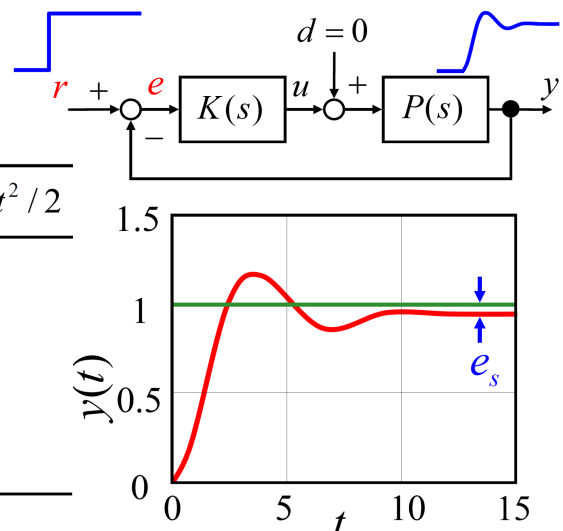
Summary: Performance Evaluation

- Transient characteristics
- Steady-state characteristics**

$$L(s) = P(s)K(s)$$

$$e_s = \frac{1}{1+L(0)} \quad K_p = L(0)$$

System type	$r(t) = 1$	$r(t) = t$	$r(t) = t^2 / 2$
0 Type	$\frac{1}{1+K_p}$	∞	∞
1 Type	0	$\frac{1}{K_v}$	∞
2 Type	0	0	$\frac{1}{K_a}$

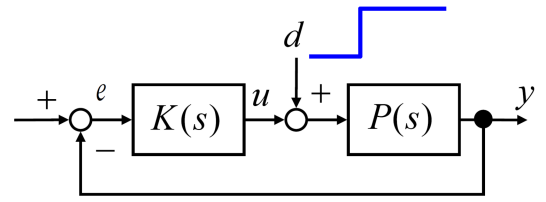


System Response

- **Zero-Input Response:** $r = 0$ $d(s) = \frac{1}{s}$

$$e(s) = -y(s) = -\frac{P(s)}{1+L(s)}d(s)$$

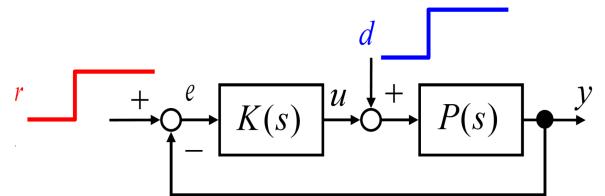
$$\Rightarrow \lim_{t \rightarrow \infty} e(t) = -\lim_{t \rightarrow \infty} y(t) = -\lim_{s \rightarrow 0} sy(s) = -\frac{P(0)}{1+L(0)}$$



- **Non-Zero Input and Disturbance Response:**

$$e(s) = \frac{1}{1+L(s)}r(s) - \frac{P(s)}{1+L(s)}d(s)$$

$$\Rightarrow \lim_{t \rightarrow \infty} e(t) = \frac{1}{1+L(0)} - \frac{P(0)}{1+L(0)}$$



Pole and Zero

impulse response transfer function: $G(s)$

- **Real pole:** $-\sigma_i$ ($i = 1 \sim M$)

Example: $G(s) = \frac{1}{s+1} \Rightarrow \sigma = -1$

- **Complex conjugate pole:** $-\alpha_i \pm j\omega_i$ ($i = 1 \sim N$)

Example: $G(s) = \frac{1}{s^2 + s + 1} \Rightarrow \frac{-1 \pm j\sqrt{3}}{2} \Rightarrow \begin{matrix} \alpha = \frac{-1}{2} \\ \omega = \frac{\sqrt{3}}{2} \end{matrix}$

System (Impulse) Response

$$y(s) = G(s) = \sum_{i=1}^M \frac{A_i}{s + \sigma_i} + \sum_{i=1}^N \frac{B_i}{(s + \alpha_i)^2 + \omega_i^2}$$

○ **Impulse response**

$$y(t) = \sum_{i=1}^M A_i e^{-\sigma_i t} + \sum_{i=1}^N \frac{B_i}{\omega_i} e^{-\alpha_i t} \sin \omega_i t$$

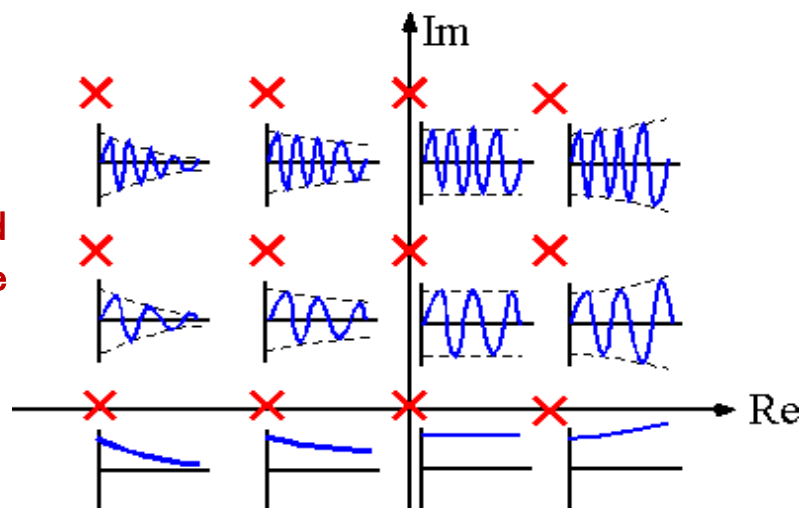


Example: $G(s) = \frac{1}{s^2 + s + 1} = \frac{1}{(s + \frac{1}{2})^2 + \frac{3}{4}} = \frac{1}{(s + \frac{1}{2})^2 + (\frac{\sqrt{3}}{2})^2}$

Poles and System Response

- The size of the real part of the pole: ⇒ Convergence speed
- The size of the imaginary part of the pole: ⇒ Period of oscillation component

Pole position and impulse response



System (Step) Response

- Step response (Laplace transform) from partial fraction decomposition:

$$y(s) = G(s) \frac{1}{s} = \frac{A_0}{s} + \sum_{i=1}^M \frac{A_i}{s + \sigma_i} + \sum_{i=1}^N \frac{B_i}{(s + \alpha_i)^2 + \omega_i^2}$$

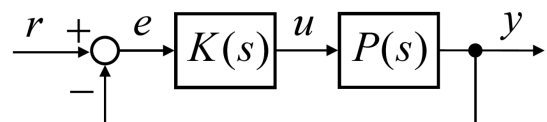
- Step response

$$y(t) = \underbrace{A_0}_{\text{---}} + \sum_{i=1}^M \underbrace{A_i e^{-\sigma_i t}}_{\text{---}} + \sum_{i=1}^N \underbrace{\frac{B_i}{\omega_i} e^{-\alpha_i t} \sin \omega_i t}_{\text{---}}$$



Zeros and Poles

$$S = \frac{1}{1 + PK}, \quad T = \frac{PK}{1 + PK}$$

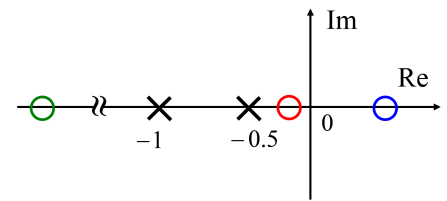


$$S(s) = \frac{1}{1 + P(s)K(s)}$$

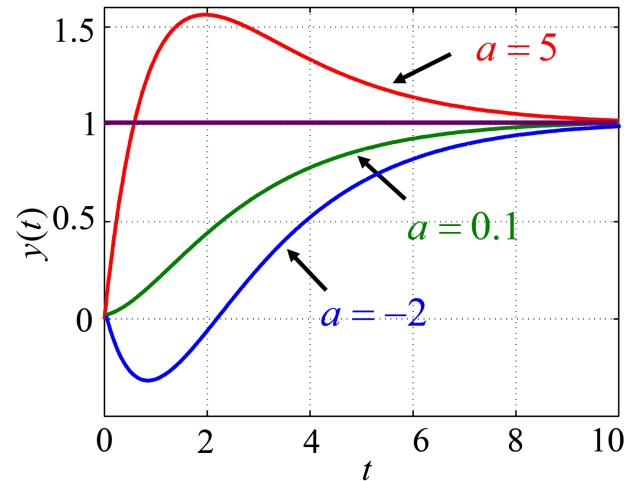
$\xrightarrow{\frac{S(p)=0}{P(p)=\infty}}$	$S(p) = \frac{1}{1 + P(p)K(p)} = 0$
$\xrightarrow{\frac{S(z)=1}{P(z)=0}}$	$S(z) = \frac{1}{1 + P(z)K(z)} = \frac{1}{1} = 1$

Impact of Zeros

Example: $G(s) = \frac{as + 1}{(s + 1)(2s + 1)}$ Poles: $-1, -0.5$
 Zero: $-\frac{1}{a}$

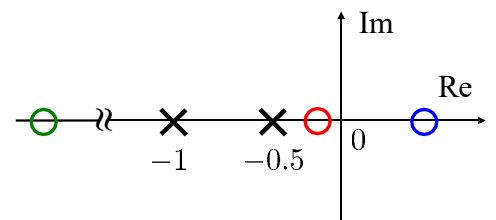


- a : Small \Rightarrow no effect
- a : Big \Rightarrow overshoot
- $a < 0$: Unstable \Rightarrow non-minimum phase

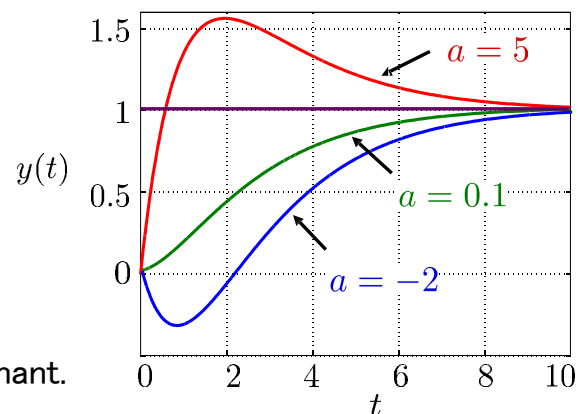


Effect of zero

Example: $G(s) = \frac{as + 1}{(s + 1)(2s + 1)}$ Poles: $-1, -0.5$
 Zero: $-\frac{1}{a}$



- $a < 0$ \Rightarrow Non-minimum phase
- a small \Rightarrow No effect
- a big \Rightarrow Overshoot

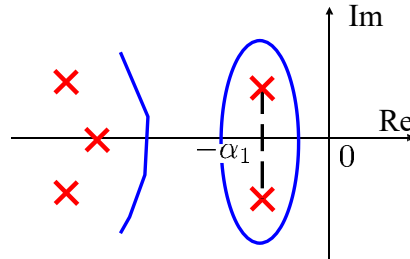


- The response of the pole near the origin is the dominant.

Dominant pole

$$y(t) = A_0 + \sum_{i=1}^M A_i e^{-\sigma_i t} + \sum_{i=1}^N \frac{B_i}{\omega_i} e^{-\alpha_i t} \sin \omega_i t$$

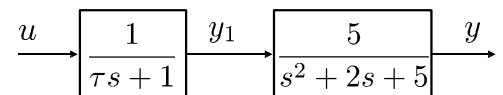
$$\left[\begin{array}{l} 0 < \alpha_1 \ll \alpha_j \quad (j = 2 \sim N) \\ 0 < \alpha_1 \ll \sigma_j \quad (j = 1 \sim M) \end{array} \right.$$



$e^{-\alpha_j t}, e^{-\sigma_j t}$ Decreases rapidly
 The slowest mode $e^{-\alpha_1 t}$ Is dominant $\Rightarrow y(t) \approx A_0 + \frac{B_1}{\omega_1} e^{-\alpha_1 t} \sin \omega_1 t$

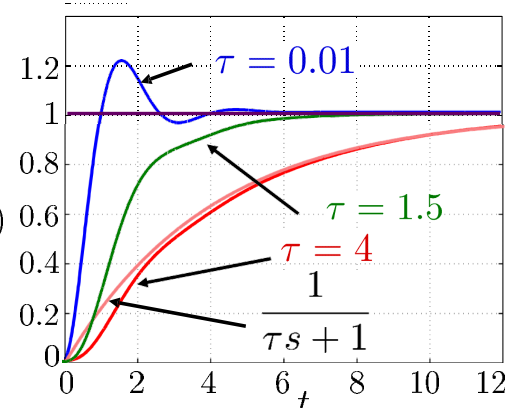
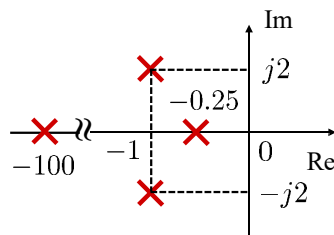
Example

$$G(s) = G_1(s)G_2(s) = \frac{1}{\tau s + 1} \cdot \frac{5}{s^2 + 2s + 5}$$



$$\left[\begin{array}{l} \tau s + 1 = 0 \Rightarrow s = -\frac{1}{\tau} \\ s^2 + 2s + 5 = 0 \Rightarrow s = -1 \pm j2 \end{array} \right.$$

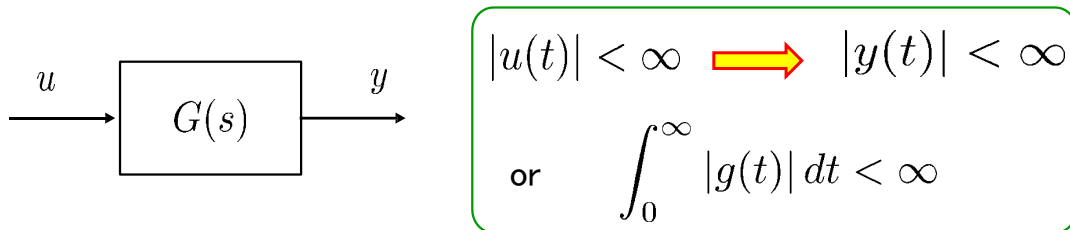
$$\begin{array}{ll} \tau = 0.01 & -\frac{1}{\tau} = -100 \quad G \approx G_2 \\ \tau = 4 & -\frac{1}{\tau} = -0.25 \quad G \approx G_1 \end{array}$$



Stability: BIBO Stability

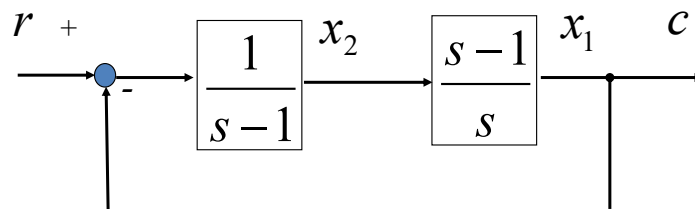
Stability: A causal, linear, time-invariant system is stable if and only if all its poles have negative real parts.

○ Bounded input bounded output (BIBO) stability



Example

Check the BIBO and internal stability of the following system:

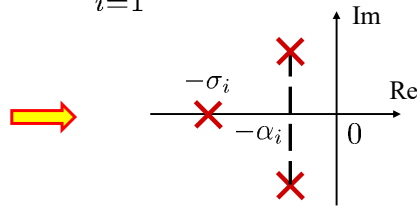


$$\frac{c(s)}{r(s)} = \frac{\frac{1}{s}}{1 + \frac{1}{s}} = \frac{1}{s+1} \implies p = -1 \implies \text{BIBO stability}$$

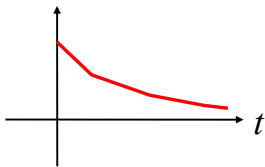
Step response (stable system)

$$y(t) = A_0 + \sum_{i=1}^M A_i e^{-\sigma_i t} + \sum_{i=1}^N \frac{B_i}{\omega_i} e^{-\alpha_i t} \sin \omega_i t$$

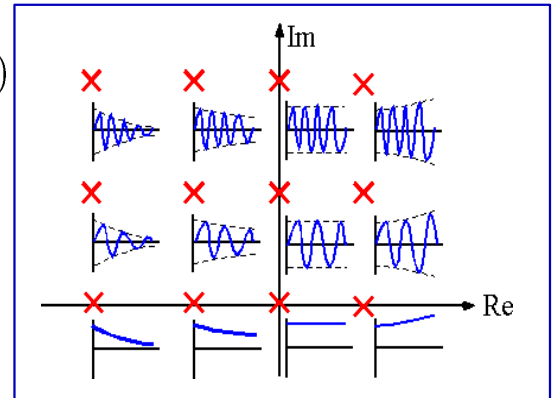
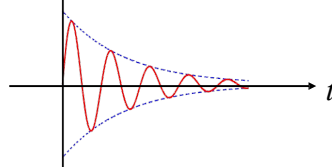
$$-\sigma_i < 0, \quad -\alpha_i < 0$$



$$e^{-\sigma_i t} \rightarrow 0 \quad (t \rightarrow \infty)$$

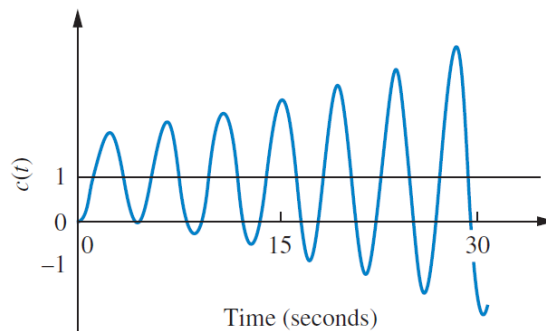
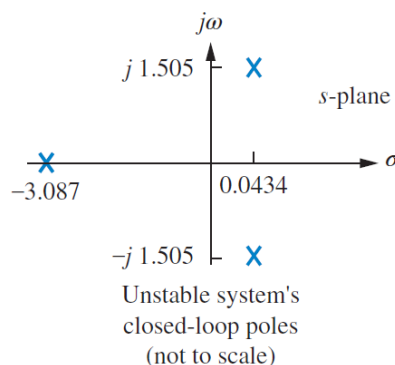
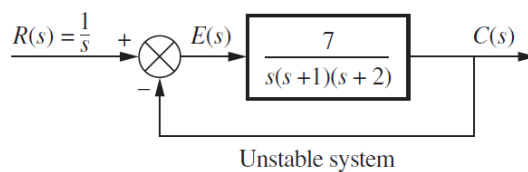


$$e^{-\alpha_i t} \sin \omega_i t \rightarrow 0 \quad (t \rightarrow \infty)$$



Step response (unstable system)

$$y(t) = A_0 + \sum_{i=1}^M A_i e^{-\sigma_i t} + \sum_{i=1}^N \frac{B_i}{\omega_i} e^{-\alpha_i t} \sin \omega_i t$$

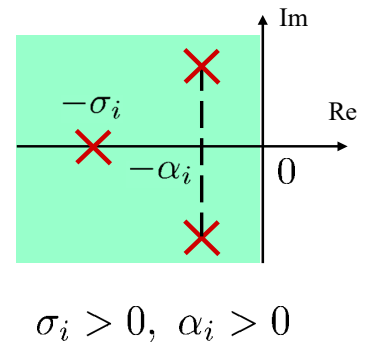


Necessary and sufficient conditions for stability

(A) Negative real parts of all poles

$$D(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0 \quad (a_n > 0)$$

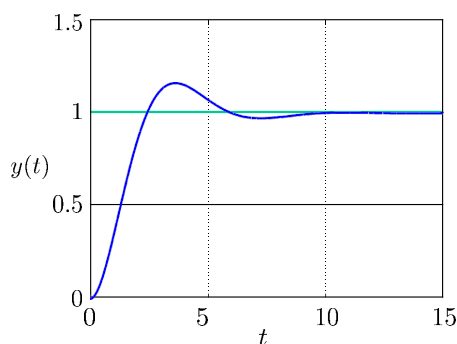
$$= a_n \prod_{i=1}^M (s + \sigma_i) \prod_{i=1}^N (s^2 + 2\alpha_i s + (\alpha_i^2 + \omega_i^2))$$



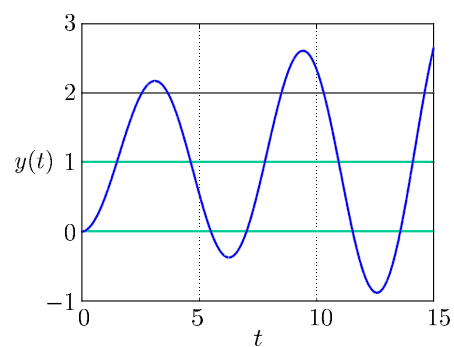
(B) All coefficients of a_n, a_{n-1}, \dots, a_0 must have same sign

Example

$$G_a(s) = \frac{1}{s^2 + s + 1}$$



$$G_b(s) = \frac{1}{s^2 - 0.1s + 1}$$



Example

$$G_1(s) = \frac{N_1(s)}{D_1(s)} \quad G_2(s) = \frac{N_2(s)}{D_2(s)}$$

$$D_1(s) = s^5 + s^4 + 3s^3 + 2s^2 + 6s + 2 \quad (\text{B: OK})$$

+1 +1 +3 +2 +6 +2

$$D_2(s) = s^5 + s^4 + 6s^3 + 3s^2 + 4s + 1 \quad (\text{B: OK})$$

+1 +1 +6 +3 +4 +1

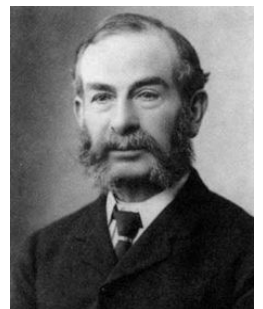
○ Are they both stable?

$$D_1(s) = 0 \quad \Rightarrow \quad \underline{0.56 \pm 1.37j}, \quad -0.89 \pm 1.33j, \quad -0.35 \quad \text{unstable}$$

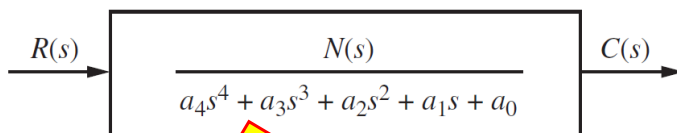
$$D_2(s) = 0 \quad \Rightarrow \quad -0.26 \pm 2.21j, \quad -0.10 \pm 0.85j, \quad -0.28 \quad \text{stable}$$

Routh's method

○ Using the "Routh Table" (1905). Then it is generalized to Routh-Hurwitz method



Example:



Routh Table:

s^4	a_4	a_2	a_0
s^3	a_3	a_1	0
s^2			
s^1			
s^0			

Routh's stability criterion

- **Completing the "Routh Table":** $D(s) = a_4s^4 + a_3s^3 + a_2s^2 + a_1s + a_0$

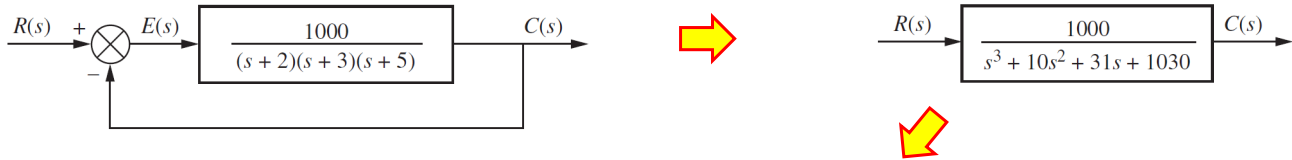
s^4	a_4	a_2	a_0
s^3	a_3	a_1	0
s^2	$-\frac{\begin{vmatrix} a_4 & a_2 \\ a_3 & a_1 \end{vmatrix}}{a_3} = b_1$	$-\frac{\begin{vmatrix} a_4 & a_0 \\ a_3 & 0 \end{vmatrix}}{a_3} = b_2$	$-\frac{\begin{vmatrix} a_4 & 0 \\ a_3 & 0 \end{vmatrix}}{a_3} = 0$
s^1	$-\frac{\begin{vmatrix} a_3 & a_1 \\ b_1 & b_2 \end{vmatrix}}{b_1} = c_1$	$-\frac{\begin{vmatrix} a_3 & 0 \\ b_1 & 0 \end{vmatrix}}{b_1} = 0$	$-\frac{\begin{vmatrix} a_3 & 0 \\ b_1 & 0 \end{vmatrix}}{b_1} = 0$
s^0	$-\frac{\begin{vmatrix} b_1 & b_2 \\ c_1 & 0 \end{vmatrix}}{c_1} = d_1$	$-\frac{\begin{vmatrix} b_1 & 0 \\ c_1 & 0 \end{vmatrix}}{c_1} = 0$	$-\frac{\begin{vmatrix} b_1 & 0 \\ c_1 & 0 \end{vmatrix}}{c_1} = 0$

Routh's stability criterion

Theorem 1:

The number of sign changes in the first column of the Routh table equals the number of roots of the polynomial in the *Right Half-Plane* (RHP).

Example



s^3	1	31	0
s^2	10 1	1030 103	0
s^1	$-\frac{\begin{vmatrix} 1 & 31 \\ 1 & 103 \end{vmatrix}}{1} = -72$	$-\frac{\begin{vmatrix} 1 & 0 \\ 0 & 0 \end{vmatrix}}{1} = 0$	$-\frac{\begin{vmatrix} 1 & 0 \\ 1 & 0 \end{vmatrix}}{1} = 0$
s^0	$-\frac{\begin{vmatrix} 1 & 103 \\ -72 & 0 \end{vmatrix}}{-72} = 103$	$-\frac{\begin{vmatrix} 1 & 0 \\ -72 & 0 \end{vmatrix}}{-72} = 0$	$-\frac{\begin{vmatrix} 1 & 0 \\ -72 & 0 \end{vmatrix}}{-72} = 0$

- **Unstable with 2 roots at the RHP**

Special Cases

- **Case 1: Zero Only in the First Column**

Solution 1: via Epsilon method

Solution 2: via Reverse coefficients

- **Case 2: Entire Row is Zero**

Solution: via an Auxiliary Polynomial for above row of zeros

Case 1: Solution 1

Example:

$$T(s) = \frac{10}{s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3}$$

s^5	1	3	5
s^4	2	6	3
s^3	0	$\frac{7}{2}$	0
s^2	$\frac{6\epsilon - 7}{\epsilon}$	3	0
s^1	$\frac{42\epsilon - 49 - 6\epsilon^2}{12\epsilon - 14}$	0	0
s^0	3	0	0

Continue

Example: $T(s) = \frac{10}{s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3}$

				$\epsilon = +$	$\epsilon = -$
s^5	1	3	5	+	+
s^4	2	6	3	+	+
s^3	0 ϵ	$\frac{7}{2}$	0	+	-
s^2	$\frac{6\epsilon - 7}{\epsilon}$	3	0	-	+
s^1	$\frac{42\epsilon - 49 - 6\epsilon^2}{12\epsilon - 14}$	0	0	+	+
s^0	3	0	0	+	+

○ **Unstable with 2 roots at the RHP**

Case 1: Solution 2

Method logic: $s^n + a_{n-1}s^{n-1} + \dots + a_1s + a_0 = 0$

- If s is replaced by $1/d$

$$\left(\frac{1}{d}\right)^n + a_{n-1}\left(\frac{1}{d}\right)^{n-1} + \dots + a_1\left(\frac{1}{d}\right) + a_0 = 0$$



$$\begin{aligned} &\left(\frac{1}{d}\right)^n \left[1 + a_{n-1}\left(\frac{1}{d}\right)^{-1} + \dots + a_1\left(\frac{1}{d}\right)^{(1-n)} + a_0\left(\frac{1}{d}\right)^{-n} \right] \\ &= \left(\frac{1}{d}\right)^n \boxed{1 + a_{n-1}d + \dots + a_1d^{(n-1)} + a_0d^n} = 0 \end{aligned}$$

Case 1: Solution 2

Example: $T(s) = \frac{10}{s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3}$

$D(s) = 3s^5 + 5s^4 + 6s^3 + 3s^2 + 2s + 1$

s^5	3	6	2
s^4	5	3	1
s^3	4.2	1.4	
s^2	1.33	1	
s^1	-1.75		
s^0	1		

- **Unstable with 2 roots at the RHP**

Case 2

Example: $T(s) = \frac{10}{s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56}$

s^5	1	6	8
s^4	1	6	8
s^3	0	0	0
s^2			
s^1			
s^0			

$P(s) = s^4 + 6s^2 + 8 \quad \Rightarrow \quad \frac{dP(s)}{ds} = 4s^3 + 12s + 0$

Continue

Example: $T(s) = \frac{10}{s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56}$

s^5	1	6	8
s^4	7 1	42 6	56 8
s^3	0 4 1	0 12 3	0 0 0
s^2	3	8	0
s^1	$\frac{1}{3}$	0	0
s^0	8	0	0

$P(s) = s^4 + 6s^2 + 8 \quad \Rightarrow \quad \frac{dP(s)}{ds} = 4s^3 + 12s + 0$

○ **Stable**

Case 2

- The order of auxiliary polynomial shows the number of poles on the $j\omega$ -axis.

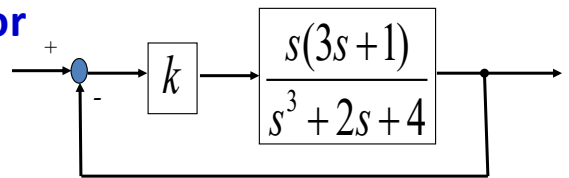
$$P(s) = s^4 + 6s^2 + 8$$



4 poles on the $j\omega$ -axis

Example

- Check the stability of following system for different values of k



$$M(s) = \frac{k \frac{s(3s+1)}{s^3+2s+4}}{1 + k \frac{s(3s+1)}{s^3+2s+4}} = \frac{ks(3s+1)}{s^3+2s+4+ks(3s+1)}$$



$$s^3 + 3ks^2 + (2+k)s + 4 = 0$$

s^3	1	2+k
s^2	3k	4
s^1	$\frac{3k(2+k)-4}{3k}$	0
s^0	4	0



$$\begin{matrix} 3k > 0 \\ \frac{3k^2 + 6k - 4}{3k} > 0 \end{matrix}$$



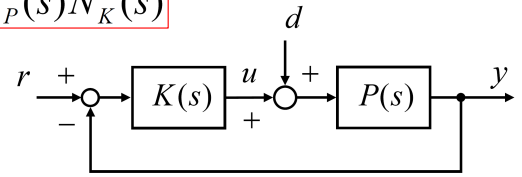
For stability:
 $k > 0.528$

Pole-Zero Cancellation

$$P(s) = \frac{N_P(s)}{D_P(s)}, \quad K(s) = \frac{N_K(s)}{D_K(s)} \quad \Rightarrow \quad \phi(s) := D_P(s)D_K(s) + N_P(s)N_K(s)$$

$$G_{ur} = \frac{D_P(s)N_K(s)}{\phi(s)} \quad G_{ud} = \frac{-N_P(s)N_K(s)}{\phi(s)}$$

$$G_{yr} = \frac{N_P(s)N_K(s)}{\phi(s)} \quad G_{yd} = \frac{N_P(s)D_K(s)}{\phi(s)}$$



Example:

$$P(s) = \frac{1}{s-1} \quad K(s) = \frac{s-1}{s}$$

$$\phi(s) = (s-1) \cdot s + 1 \cdot (s-1) = \underline{(s-1)}(s+1) = 0 \quad \Rightarrow \quad G_{yr}(s) = \frac{P(s)K(s)}{1+P(s)K(s)} = \frac{\cancel{s-1}}{\cancel{(s-1)}(s+1)}$$

Continue

$$P(s) = \frac{1}{s-1}, \quad K(s) = \frac{s-1}{s} = 1 - \frac{1}{s} \quad \Rightarrow \quad P(s)K(s) = \frac{1}{\cancel{s-1}} \cdot \frac{\cancel{s-1}}{s} = \frac{1}{s}$$

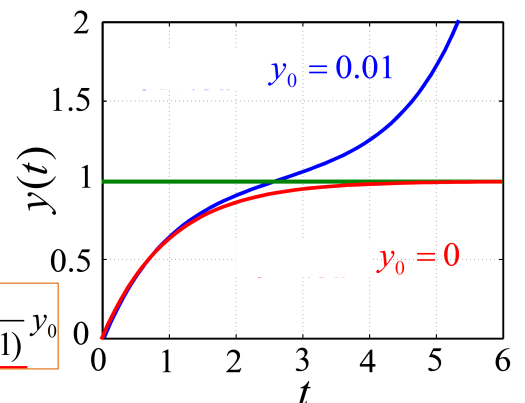
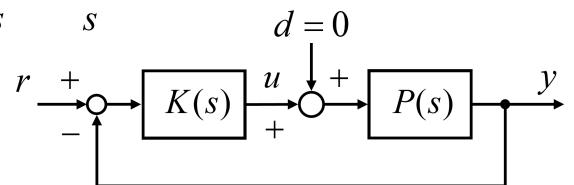
$$y(s) = \frac{P(s)K(s)}{1+P(s)K(s)} \cdot r(s) = \frac{\frac{1}{s}}{1+\frac{1}{s}} \cdot r(s) = \frac{1}{\underline{s+1}} \cdot r(s)$$

$$P(s) = \frac{y(s)}{u(s)} = \frac{1}{s-1} \quad \Rightarrow \quad (s-1)y(s) = u(s)$$

$$\dot{y}(t) - y(t) = u(t)$$

$$(sy(s) - y_0) - y(s) = u(s) \quad \Rightarrow \quad y(s) = \frac{1}{s-1}u(s) + \frac{1}{s-1}y_0$$

$$y(s) = \frac{1}{\cancel{s-1}} \cdot \frac{\cancel{s-1}}{s} (r(s) - y(s)) + \frac{1}{s-1}y_0 \quad \Rightarrow \quad y(s) = \frac{1}{s+1}r(s) + \frac{s}{(s+1)(s-1)}y_0$$



Internal Stability

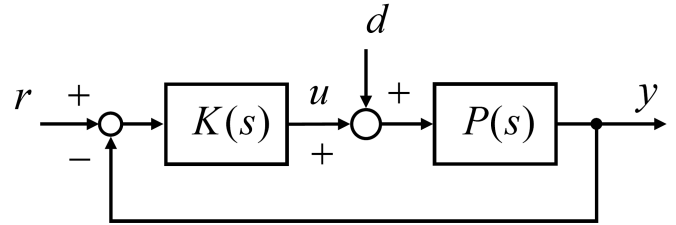
Internal Stability: A system is internally stable if and only if the poles of all possible transfer functions have negative real parts.

$$G_{ur}(s) = \frac{K(s)}{1 + P(s)K(s)}$$

$$G_{ud}(s) = \frac{-P(s)K(s)}{1 + P(s)K(s)}$$

$$G_{yr}(s) = \frac{P(s)K(s)}{1 + P(s)K(s)}$$

$$G_{yd}(s) = \frac{P(s)}{1 + P(s)K(s)}$$



Asymptotic Stability

Asymptotic Stability: A system is asymptotically stable if and only if the all eigenvalues have negative real parts.

○ How can we check asymptotic stability?

Let $|sI - A| = 0 \Rightarrow$ Find eigenvalues $\lambda_1, \lambda_2, \dots, \lambda_n$

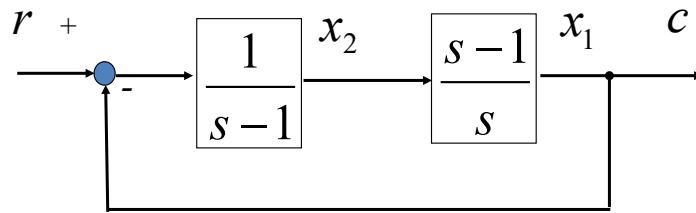
If $\lambda_1, \lambda_2, \dots, \lambda_n \in \text{LHP}$



System is asymptotically stable

Example

- Check the Asymptotic/Internal stability of the following system:



$$\begin{aligned} \dot{x}_2 - x_2 &= r - x_1 & \dot{x}_1 &= -x_1 + r \\ \dot{x}_1 &= \dot{x}_2 - x_2 & & \end{aligned} \Rightarrow \dot{x}_2 = -x_1 + x_2 + r \Rightarrow \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} r$$

$$|sI - A| = \begin{vmatrix} s+1 & 0 \\ 1 & s-1 \end{vmatrix} = s^2 - 1 = 0 \Rightarrow \lambda_1 = 1 \quad \lambda_2 = -1$$

⇒ **Not Asympt. Stability**

Thank You!

